

Energy Harvesting from Ambient Vibrations Frédéric Giraud

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Energy Harvesting from Ambient Vibrations

Frédéric Giraud

L2EP – University Lille1

November 27, 2012

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Table of contents

[Introduction](#page-3-0)

- [What is Energy Harvesting ?](#page-3-0)
- **[Generator Technologies](#page-7-0)**
- **•** [Summary](#page-12-0)

2 [Modelling of a piezoelectric energy harvester](#page-14-0)

- [Presentation of the system](#page-14-0)
- [EMR of the system](#page-16-0)
- **[Power Extraction on a load resistor](#page-17-0) R_L** from harmonic oscillation

3 [An Example of inverter](#page-30-0)

- **•** [Introduction](#page-30-0)
- **[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0)**

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

What is Energy Harvesting ?

We extract energy from an *ambient and free source:*

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

What is Energy Harvesting ?

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

4 **ED**

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We extract energy from an *ambient and free source:*

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

4 **ED**

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

4 **ED**

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

What is Energy Harvesting ?

We extract energy from an *ambient and free source:*

We talk about Energy Harvesting *or also* energy scavenging *when the converted power is small, typically less than* 1*W .*

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

What is Energy Harvesting ?

We extract energy from an *ambient and free source:*

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Objectives: Sensors Network

www.perpetuum.com

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Gutiérriez, A Heterogeneous Wireless Identification Network for the Localization of Animals Based on Stochastic Movements

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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http://www.rfwirelesssensors.com, 2012
Continous Power / cm³ vs. Life for Several Power Sources

Roundy et Al.:A study of low level vibrations as a power source for wireless sensor nodes.

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Objectives: Power, just where you need it

http://enocean.com

- \bullet Wireless
- ۰ Reduce Cost, and is reconfigurable
- **Better Waste Cycle** (Information from Enocean)

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

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Innowattech's systems produces power with vehicles

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http://www.innowattech.com

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 QQ

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

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 Ω

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

Objectives: Marketing Purpose

Experience: Same Remote controller energized by human power, but with different packaging.

"No need for Batteries"

4 **ED**

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

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54% of people Will choose the first one because it is eco-friendly. (Jansen, Human power empirically explored)

4 **ED**

 QQ

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

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Several projects are born from this fact: **Metis** Produces energy from dancers' movements.

In Toulouse, the system VIHA proposes Smart Tiles to energies street lights.

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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The energy converter

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

4 0 8

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э

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

4 0 8

The energy converter

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

The energy converter

4 0 8

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

Solar Harvesters:

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Solar Harvesters:

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

This sensor measures IntraOccular Pressure http://cymbet.com

Handbag to recharge electronic devices http://www.neubers.de

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Solar Harvesters:

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Handbag to recharge electronic devices http://www.neubers.de

Power and current as a function of voltage:

Solar Energy Harvester Evaluation Kit http://ti.com

 QQ

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Solar Harvesters:

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

4 0 8

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 QQ

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Thermoelectric

A Peltier module from http://www.tellurex.com R_{DC}

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Thermoelectric

A Peltier module from http://www.tellurex.com R_{DC} I_{DC}

Temperature Gradient (residential). Lindsay Miller, http://uc-ciee.org
Clamp-on Drain Harvester

plumbing application from http://www.nextreme.com

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Magnetic

1) Diode turns ON

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Magnetic

1) Diode turns ON 2) $\frac{di}{dt} = 0$ because $e - v_B = 0$

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Magnetic

- 1) Diode turns ON
- 2) $\frac{di}{dt} = 0$ because $e v_B = 0$
- 3) $i = 0$, diode turns OFF

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Magnetic

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2)
$$
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$$
 because $e - v = 0$

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Magnetic

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Magnetic

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Magnetic

 $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$ $P = \langle y_B i \rangle = v_{B} \langle i \rangle$

[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

Piezoelectric

An electronic lighter, http://freepatentsonline.com

Piezoelectric crystals

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Piezoelectric crystals Cantilever beam

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Equivalent electrical circuit

i^m is a current proportional to the deformation speed

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

An electronic lighter, http://freepatentsonline.com

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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Piezoelectric crystals Cantilever beam

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

An electronic lighter, http://freepatentsonline.com

Piezoelectric crystals Cantilever beam

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

An electronic lighter, http://freepatentsonline.com

Piezoelectric crystals Cantilever beam

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

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[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

Piezoelectric

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0)

An electronic lighter, http://freepatentsonline.com

Piezoelectric crystals Cantilever beam

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0) [What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

There is no "one fit all" solution

Each solution may be efficient in a certain range of Power.

Meanwhile, shrinking Chips consumption come at a time when energy har[vesti](#page-65-0)n[g b](#page-40-0)[ec](#page-39-0)[omes](#page-40-0) [effi](#page-33-0)[c](#page-34-0)[ient](#page-40-0) [an](#page-29-0)[d](#page-30-0) [pra](#page-40-0)[ctic](#page-1-0)[al](#page-40-0) (source: IDtechex.com) 4 ロ ト 4 何 ト 4 ラ ト 4 ラ

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[Modelling of a piezoelectric energy harvester](#page-14-0) [An Example of inverter](#page-30-0)

[What is Energy Harvesting ?](#page-3-0) [Generator Technologies](#page-7-0) [Summary](#page-12-0)

Table of contents

[Introduction](#page-3-0)

- What is Energy Harvesting?
- **[Generator Technologies](#page-7-0)**
- **•** [Summary](#page-12-0)

2 [Modelling of a piezoelectric energy harvester](#page-14-0)

- [Presentation of the system](#page-14-0)
- [EMR of the system](#page-16-0)
- **[Power Extraction on a load resistor](#page-17-0) R_L** from harmonic oscillation

3 [An Example of inverter](#page-30-0)

- [Introduction](#page-30-0)
- **[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0)**

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

Coordinates and assumptions

4 0 8

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

Coordinates and assumptions

 \bullet The bender is attached to a vibrating and rigid case,

4 0 8

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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Frédéric Giraud [Master E2D2](#page-1-0) November 27, 2012 14 / 40

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Equations

• Dynamic of the mass M: Glossary

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- f . the force onto M 0
- \bullet A, vibration's amplitude
- \bullet ω , vibration's pulsation
- \bullet f_{acc} is the inertial force
- \bullet i current of the device (actuator convention)
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• These actions are opposite to the PE effect: $f = f_n - f_s$

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EMR of the system

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v = \frac{i}{C_b} \sqrt{\frac{v}{i_m}}
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i_m = Nv, \quad i_m = Nw
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Asumption

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\left\{\begin{array}{c}\n\downarrow \\
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\downarrow \\
\downarrow\n\end{array}\right\}
$$
\nAnd $R_L \ll \frac{1}{C_b\omega}$, yields\n
$$
v \simeq -R_L i_m
$$

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For an ideal generator $(D_s = 0)$

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- $M\ddot{\underline{w}} + N^2 R_L \dot{\underline{w}} + K_s \underline{w} = \underline{f}_{acc}$ $\longrightarrow R_L$ acts as a damping
- $P_2 = -\frac{1}{2}R_L|i_m|^2$

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For an ideal generator $(D_s = 0)$

- $M\underline{\ddot{w}} = \underline{f} + \underline{f}_{acc}$
- \bullet *f* = *N*_{*v*} $-$ *K*_s*w*

$$
\bullet \ \underline{v} = -R_L \underline{i}_m = -R_L N \underline{\dot{w}}
$$

•
$$
M\underline{\ddot{w}} + N^2 R_L \underline{\dot{w}} + K_s \underline{w} = \underline{f}_{acc}
$$

\n $\longrightarrow R_L$ acts as a damping

$$
\bullet \ \ P_2 = -\tfrac{1}{2}R_L|i_m|^2
$$

$$
\bullet \ \ |i_m| = N|\dot{w}| = \frac{\omega.N.|f_{acc}|}{\sqrt{(K_s - M\omega^2)^2 + (N^2R_L\omega)^2}}
$$

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For an ideal generator $(D_s = 0)$

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P_2 = -\frac{1}{2} \frac{N^2 R_L \omega^2 |f_{acc}|^2}{(K_s - M \omega^2)^2 + (N^2 R_L \omega)^2}
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For an ideal generator $(D_s = 0)$

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\n- \n
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\n
\n- \n $P_2 = -\frac{1}{2} \frac{N^2 R_L \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + (N^2 R_L \omega)^2}$ \n
\n

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 QQ

For an ideal generator $(D_s = 0)$

- $M\ddot{w} = f + f_{acc}$
- \bullet *f* = *Nv* − *K_sw*

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\bullet \ \underline{v} = -R_L \underline{i}_m = -R_L N \underline{\dot{w}}
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 $M\ddot{\underline{w}} + N^2 R_L \dot{\underline{w}} + K_s \underline{w} = \underline{f}_{acc}$ $\longrightarrow R_L$ acts as a damping

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\n

4 D F

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P_{2Max} = \frac{(MA\omega^2)^2}{2N^2R_L}
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We can harvest as much power as we want

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\bullet \ \ P_{2Max} = \frac{(MA\omega^2)^2}{2N^2R_L}, \ W_{max} = \frac{MA\omega}{N^2R_L}
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We can harvest as much power as we want, at the expense of large displacement of the bender's tip

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For an ideal generator $(D_s = 0)$

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4 D F

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P_{2Max} = \frac{(MA\omega^2)^2}{2N^2R_L}
$$
, $W_{max} = \frac{MA\omega}{N^2R_L}$,
 $v_{max} = \frac{MA\omega^2}{N}$

We can harvest as much power as we want, at the expense of large displacement of the bender's tip

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$$

$$
v_{max} = \frac{MA\omega^2}{N}
$$

$$
\bullet \ \ P_{1Max} = \frac{1}{2} f_{acc} \omega W_{Max} = \frac{(M A \omega^2)^2}{N^2 R_L} = P_{2Max}
$$

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We can harvest as much power as we want, at the expense of large displacement of the bender's tip

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November 27, 2012 18 / 40

For an ideal generator $(D_s = 0)$

•
$$
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$$
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•
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\bullet \ \ P_{2Max} = \frac{(MA\omega^2)^2}{2N^2R_L}, \ W_{max} = \frac{MA\omega}{N^2R_L},
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November 27, 2012 18 / 40

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

$$
\bullet \ \underline{f} = N\underline{v} - K_s\underline{w} - D_s\underline{\dot{w}}
$$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

$$
\begin{aligned}\n\bullet \quad & \underline{f} = N\underline{v} - K_s \underline{w} - D_s \underline{w} \\
\bullet \quad & \underline{w} = \frac{f_{\text{acc}}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_L)}\n\end{aligned}
$$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- $$
f = N\underline{v} - K_s\underline{w} - D_s\underline{w}
$$
\n- $\underline{w} = \frac{f_{\text{acc}}}{(K_s - M\omega^2) + j\omega(D_s + N^2R_l)}$
\n- $P_2 = -\frac{1}{2}R_L|i_m|^2$
\n

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\begin{aligned}\n \bullet \quad & \underline{f} = N\underline{v} - K_s \underline{w} - D_s \underline{\dot{w}} \\
 \bullet \quad & \underline{w} = \frac{f_{acc}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_L)} \\
 \bullet \quad & P_2 = -\frac{1}{2} R_L |i_m|^2 \\
 \bullet \quad & P_2 = -\frac{1}{2} \frac{R_L N^2 \omega^2 |f_{acc}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2}\n \end{aligned}
$$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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\begin{aligned}\n \bullet \quad & \underline{f} = N\underline{v} - K_s \underline{w} - D_s \underline{\dot{w}} \\
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 \bullet \quad & P_2 = -\frac{1}{2} \frac{R_L N^2 \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)} \\
 \bullet \quad & P_1 = -\frac{1}{2} \Re(f_{\text{acc}} \cdot \underline{\dot{w}}^*)\n \end{aligned}
$$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- $$
f = N\underline{v} - K_s\underline{w} - D_s\underline{w}
$$
\n- $$
\underline{w} = \frac{f_{acc}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_L)}
$$
\n- $$
P_2 = -\frac{1}{2}R_L|i_m|^2
$$
\n- $$
P_2 = -\frac{1}{2}\frac{R_L N^2 \omega^2 |f_{acc}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2}
$$
\n- $$
P_1 = -\frac{1}{2}\Re(\underline{f_{acc} \cdot \underline{w}}^*)
$$
\n- $$
P_1 = -\frac{1}{2}\frac{(D_s + R_L N^2)\omega^2 |f_{acc}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2}
$$
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
$$
\begin{aligned}\n \mathbf{O} \quad & \mathbf{f} = N\underline{V} - K_s\underline{w} - D_s\underline{\dot{w}} \\
 \mathbf{O} \quad & \underline{w} = \frac{f_{\text{acc}}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_l)} \\
 \mathbf{O} \quad & P_2 = -\frac{1}{2}R_L|i_m|^2 \\
 \mathbf{O} \quad & P_2 = -\frac{1}{2}\frac{R_L N^2 \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_l)^2} \\
 \mathbf{O} \quad & P_1 = -\frac{1}{2}\Re(\underline{f_{\text{acc}}}\cdot\underline{\dot{w}}^*) \\
 \mathbf{O} \quad & P_1 = -\frac{1}{2}\frac{(D_s + R_L N^2)\omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_l)^2}\n \end{aligned}
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- $$
\begin{aligned}\n\mathbf{O} \quad & \mathbf{f} = N\underline{V} - K_s\underline{w} - D_s\underline{\dot{w}} \\
\mathbf{O} \quad & \underline{w} = \frac{f_{\text{acc}}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_l)} \\
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\mathbf{O} \quad & P_1 = -\frac{1}{2}\Re(\underline{f_{\text{acc}}}\cdot \underline{\dot{w}}^*) \\
\mathbf{O} \quad & P_1 = -\frac{1}{2}\frac{(D_s + R_L N^2)\omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_l)^2}\n\end{aligned}
$$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
$$
\begin{aligned}\n \Phi \, & \, \underline{f} = N\underline{v} - K_s \underline{w} - D_s \underline{\dot{w}} \\
 \Phi \, & \underline{w} = \frac{f_{\text{acc}}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_L)} \\
 \Phi \, & P_2 = -\frac{1}{2} R_L |i_m|^2 \\
 \Phi \, & P_2 = -\frac{1}{2} \frac{R_L N^2 \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2} \\
 \Phi \, & P_1 = -\frac{1}{2} \Re(f_{\text{acc}} \cdot \underline{\dot{w}}^*) \\
 \Phi \, & P_1 = -\frac{1}{2} \frac{(D_s + R_L N^2) \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2}\n \end{aligned}
$$
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 ω_0 should still be the vibration's pulsation.

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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\begin{aligned}\n \Phi \, & \, \underline{f} = N\underline{v} - K_s \underline{w} - D_s \underline{\dot{w}} \\
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 \Phi \, & P_2 = -\frac{1}{2} R_L |i_m|^2 \\
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 \Phi \, & P_1 = -\frac{1}{2} \frac{(D_s + R_L N^2) \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2}\n \end{aligned}
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\n
\n

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
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\begin{aligned}\n \Phi \, & \, \underline{f} = N\underline{v} - K_s \underline{w} - D_s \underline{\dot{w}} \\
 \Phi \, & \underline{w} = \frac{f_{\text{acc}}}{(K_s - M\omega^2) + j\omega(D_s + N^2 R_L)} \\
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 \Phi \, & P_1 = -\frac{1}{2} \frac{(D_s + R_L N^2) \omega^2 |f_{\text{acc}}|^2}{(K_s - M\omega^2)^2 + \omega^2(D_s + N^2 R_L)^2}\n \end{aligned}
$$
\n
\n

 ω_0 should still be the vibration's pulsation.

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
$$
\begin{aligned}\n \Phi \, &= N \underline{v} - K_s \underline{w} - D_s \underline{w} \\
 \Phi \, &= \frac{f_{\text{acc}}}{(K_s - M \omega^2) + j \omega (D_s + N^2 R_L)} \\
 \Phi \, &P_2 = -\frac{1}{2} R_L |i_m|^2 \\
 \Phi \, &P_2 = -\frac{1}{2} \frac{R_L N^2 \omega^2 |f_{\text{acc}}|^2}{(K_s - M \omega^2)^2 + \omega^2 (D_s + N^2 R_L)^2} \\
 \Phi \, &P_1 = -\frac{1}{2} \Re \left(\frac{D_s + R_L N^2}{K_s - M \omega^2} \right)^2 + \omega^2 (D_s + N^2 R_L)^2\n \end{aligned}
$$
\n
\n

 ω_0 should still be the vibration's pulsation.

•
$$
W_{max} = \frac{|f_{acc}|}{(D_s + N^2 R_L)\omega_0}
$$
, $P_{1max} = \frac{1}{2} \frac{|f_{acc}|^2}{D_s + N^2 R_L}$,
\n $P_{2max} = \frac{1}{2} \frac{N^2 R_L |f_{acc}^2|}{(D_s + N^2 R_L)^2}$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

•
$$
W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_s + N^2 R_L)\omega_0}
$$
, $P_{1\text{max}} = \frac{1}{2} \frac{|f_{\text{acc}}|^2}{D_s + N^2 R_L}$

$$
\bullet \ \ P_{2max} = \frac{1}{2} \frac{N^2 R_L |f_{\text{acc}}|^2}{(D_s + N^2 R_L)^2}
$$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
$$
W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_s + N^2 R_L)\omega_0}, \quad\n P_{1\text{max}} = \frac{1}{2} \frac{|f_{\text{acc}}|^2}{D_s + N^2 R_L}
$$
\n
\n- \n
$$
P_{2\text{max}} = \frac{1}{2} \frac{N^2 R_L |f_{\text{acc}}|^2}{(D_s + N^2 R_L)^2}
$$
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
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$$
\n
\n- \n
$$
P_{2\text{max}} = \frac{1}{2} \frac{N^2 R_l |f_{\text{acc}}|^2}{(D_s + N^2 R_l)^2}
$$
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\n

When $R_L \searrow R_1 \nearrow$, which is good, but the losses increase as well: it exists an optimal value of R_L which optimizes P_2 for a given vibration amplitude.

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
$$
W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_s + N^2 R_L) \omega_0}, \quad\n P_{1\text{max}} = \frac{1}{2} \frac{|f_{\text{acc}}|^2}{D_s + N^2 R_L}
$$
\n
\n- \n
$$
P_{2\text{max}} = \frac{1}{2} \frac{N^2 R_L |f_{\text{acc}}|^2}{(D_s + N^2 R_L)^2}
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\n
\n

When $R_1 \searrow R_1 \nearrow$, which is good, but the losses increase as well: it exists an optimal value of R_L which optimizes P_2 for a given vibration amplitude. It can be shown:

 $R_{Lopt} = \frac{D_s}{N^2}$ $P_{2opt} = \frac{|f_{acc}|^2}{8D_e}$ 8 $D_{\rm s}$ $P_{1opt} = \frac{|f_{acc}|^2}{4D_e}$ $\frac{q_{acc\perp}}{4D_s} = 2.P_{2opt}$

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
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W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_s + N^2 R_l) \omega_0}, \quad\n P_{1\text{max}} = \frac{1}{2} \frac{|f_{\text{acc}}|^2}{D_s + N^2 R_l}
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\n
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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\n- \n
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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\n- \n
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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\n
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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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- voltage is not so high.

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real generator $(D_s \neq 0)$

\n- \n
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\n
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- voltage is not so high.

Example

Device's properties

$$
N = 0.012N/V, K_s = 6300N/m, C_b = 300nF, D_s = 0.17Ns/m, M = 1g
$$

Calculate for $A = 0.1$ *mm*

- the best working frequency,
- \bullet the harvested P_2 power in the best case,
- \bullet the power of the source P_1 in such best case,
- \bullet the optimal resistor R_L ,
- the deflection amplitude of the bender,
- \bullet the voltage for this working point.

Validation

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 Is *v* = −*R*_L i_m a valid assumption?

• The best working frequency is given by

$$
f_0 = \frac{1}{2\pi} \sqrt{\frac{K_s}{M}} = \frac{1}{2\pi} \sqrt{\frac{6300}{1.10^{-3}}} = \frac{400 \, Hz}{}
$$

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• The best working frequency is given by

$$
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$$

• For the best case,
$$
P_2
$$
 is given by
\n
$$
P_2 = \frac{|f_{acc}|^2}{8D_s} = \frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)^2}{8.0.17} = \frac{464mW}{}
$$

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э

• The best working frequency is given by

$$
f_0 = \frac{1}{2\pi} \sqrt{\frac{K_s}{M}} = \frac{1}{2\pi} \sqrt{\frac{6300}{1.10^{-3}}} = \frac{400 \, Hz}{}
$$

• For the best case,
$$
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\n
$$
P_2 = \frac{|f_{acc}|^2}{8D_s} = \frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)^2}{8.0.17} = \frac{464mW}{}
$$

• For the best case $P_1 = 2.P_2 = \frac{928mW}{9}$

 \leftarrow

• The best working frequency is given by

$$
f_0 = \frac{1}{2\pi} \sqrt{\frac{K_s}{M}} = \frac{1}{2\pi} \sqrt{\frac{6300}{1.10^{-3}}} = \frac{400 \, Hz}{}
$$

• For the best case,
$$
P_2
$$
 is given by
\n
$$
P_2 = \frac{|f_{acc}|^2}{8D_s} = \frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)^2}{8.0.17} = \frac{464mW}{}
$$

• For the best case $P_1 = 2.P_2 = \frac{928mW}{9}$

• The optimal resistor
$$
R_{Lopt}
$$
 is given by

$$
R_{Lopt} = \frac{D_s}{N^2} = \frac{0.17}{0.012^2} = \frac{1180\Omega}{1.012^2}
$$

4 0 8

• The best working frequency is given by

$$
f_0 = \frac{1}{2\pi} \sqrt{\frac{K_s}{M}} = \frac{1}{2\pi} \sqrt{\frac{6300}{1.10^{-3}}} = \frac{400 \, Hz}{}
$$

- For the best case, P_2 is given by $P_2 = \frac{|f_{acc}|^2}{8D_s}$ $\frac{\left|f_{acc}\right|^{2}}{8B_{s}}=\frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^{2})^{2}}{8.0,17}=464mW$
- For the best case $P_1 = 2.P_2 = 928 \text{ mW}$
- The optimal resistor R_{Lopt} is given by $R_{Lopt} = \frac{D_s}{N^2} = \frac{0.17}{0.012^2} = \frac{1180Ω}{N^2}$
- The deflection W_{max} is given by $W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_{\text{s}} + N^2 R)}$ $\frac{|f_{\rm acc}|}{(D_{\rm s}+N^2R_L)\omega_0}=\frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)}{2.0,17.2\pi.400}= \frac{738\mu m!}{1500}$

• The best working frequency is given by

$$
f_0 = \frac{1}{2\pi} \sqrt{\frac{K_s}{M}} = \frac{1}{2\pi} \sqrt{\frac{6300}{1.10^{-3}}} = \frac{400 \, Hz}{}
$$

For the best case,
$$
P_2
$$
 is given by
\n
$$
P_2 = \frac{|f_{acc}|^2}{8D_s} = \frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)^2}{8.0.17} = \frac{464mW}{}
$$

• For the best case $P_1 = 2.P_2 = 928 \text{mW}$

- The optimal resistor R_{Lopt} is given by $R_{Lopt} = \frac{D_s}{N^2} = \frac{0.17}{0.012^2} = \frac{1180Ω}{N^2}$
- The deflection W_{max} is given by $W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_{\text{s}} + N^2 R)}$ $\frac{|f_{\rm acc}|}{(D_{\rm s}+N^2R_L)\omega_0}=\frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)}{2.0,17.2\pi.400}= \frac{738\mu m!}{1500}$
- The voltage is then given by

$$
v_{max} = NR_{L}\omega_{0}|\underline{w}| = 0,012.1180.2\pi.400.738.10^{-6} = \underline{26V}
$$

 Ω

• The best working frequency is given by

$$
f_0 = \frac{1}{2\pi} \sqrt{\frac{K_s}{M}} = \frac{1}{2\pi} \sqrt{\frac{6300}{1.10^{-3}}} = \frac{400 \, Hz}{}
$$

• For the best case,
$$
P_2
$$
 is given by

$$
P_2 = \frac{|f_{acc}|^2}{8D_s} = \frac{(1.10^{-3}.1.10^{-4}.(2\pi.400)^2)^2}{8.0.17} = \frac{464mW}{}
$$

• For the best case
$$
P_1 = 2.P_2 = \frac{928 \, \text{mW}}{1}
$$

• The optimal resistor
$$
R_{Lopt}
$$
 is given by

$$
R_{Lopt} = \frac{D_s}{N^2} = \frac{0.17}{0.012^2} = \frac{1180\Omega}{1.002}
$$

• The deflection
$$
W_{\text{max}}
$$
 is given by
\n
$$
W_{\text{max}} = \frac{|f_{\text{acc}}|}{(D_s + N^2 R_L)\omega_0} = \frac{(1.10^{-3} .1.10^{-4} . (2\pi .400)^2)}{2.0.17.2\pi .400} = \frac{738 \mu \text{m}}{2.00 \mu \text{m}^2}
$$

• The voltage is then given by

$$
v_{max} = NR_{L}\omega_{0}|\underline{w}| = 0,012.1180.2\pi.400.738.10^{-6} = \underline{26V}
$$

•
$$
Z_{Cb} = \frac{1}{C_b \omega} = \frac{1}{2\pi \cdot 400.300.10^{-9}} = \frac{1990 \Omega}{\omega} \approx R_L
$$
, \longrightarrow Calculations are NOT valid!

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

For a real Generator, $D_s \neq 0$ and $v \neq -R_L i_m$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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and we write: $\underline{v} = -j\omega Nr_{Leq}\underline{w} - Nk_{eq}\underline{w}$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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 $\omega_0 \gg \frac{1}{R_L C_b}$ ω *r*Leq|dB , *k*Leq|dB ω_0 1 $R_{L}C_{b}$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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$$
((K_s + N^2 k_e q) - M\omega^2) + j\omega (D_s + N^2 r_{\text{Leg}}) \underline{w} = \underline{f}_{acc \rightarrow \langle \text{d} \rangle \rightarrow \langle \text{d} \rangle \rightarrow \langle \text{d} \rangle}
$$

Proveer 27, 2012 23 / 40
November 27, 2012 23 / 40

Rule of the Thumb

Let R_b defined as $R_b C_b \omega_0 = 1$, $\omega_0 < \frac{1}{R_L C_b} \rightarrow R_L < R_b$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

Partial Conclusion

If $R_{opt} < R_b$

A resistor can recover the power optimally. But the study was not valid for high R_L . What happens for $R_L \gg R_b$?

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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If $R_{opt} > R_b$

The power is not well extracted because $P_2 < P_{2max}$. This happens for high damped mechanisms. A simple resistor cannot recover the power optimally (and this is due to C_h).

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

What happens if $R_{opt} < R_b$ and $R_L \gg R_b$?

resonance is shifted

\n- \n
$$
r_{Leq} = \frac{R_L}{1 + (R_L C_b \omega)^2} \simeq \frac{R_L}{(R_L C_b \omega)^2}
$$
\n
\n- \n
$$
k_{eq} = R_L \frac{\omega^2 R_L C_b}{1 + (R_L C_b \omega)^2} \simeq \frac{1}{C_b}
$$
\n
\n- \n
$$
((K_s + N^2 K_e q) - M \omega^2) + j \omega (D_s + N^2 r_{Leq}) \underline{w} = f_{acc}
$$
 leads to:\n
$$
\omega_0' = \sqrt{\frac{K_s + N^2 k_e q}{M}} = \sqrt{\frac{K_s + \frac{N^2}{C_b}}{M}}
$$
\n
\n

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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$$
\begin{aligned}\n\bullet \quad r_{Leq} &= \frac{R_L}{1 + (R_L C_b \omega)^2} \simeq \frac{R_L}{(R_L C_b \omega)^2} \\
\bullet \quad k_{eq} &= R_L \frac{\omega^2 R_L C_b}{1 + (R_L C_b \omega)^2} \simeq \frac{1}{C_b} \\
\left(\left(K_s + N^2 k_e q \right) - M \omega^2 \right) + j \omega \left(D_s + N^2 r_{Leq} \right) \underline{w} &= \underline{f}_{acc} \text{ leads to:} \\
\omega_0' &= \sqrt{\frac{K_s + N^2 k_e q}{M}} = \sqrt{\frac{K_s + \frac{N^2}{C_b}}{M}}\n\end{aligned}
$$

Another optimal resistor

The optimal power is harvested is $N^2 r_{\text{Leq}} = D_s$, leading to: N^2R_L $\frac{N^2 R_L}{(R_L C_b \omega'_0)^2} = \frac{N^2}{\frac{1}{2} N^2}$ $R_L C_b^2$ $rac{K_s + \frac{N^2}{C_b}}{M}$ $= D_s$ $R_{Lopt2} = \frac{N^2}{D_s}$ $rac{N^2}{D_s} \frac{1}{C^2 \frac{K_s}{c^2 (1 - \frac{N_s}{c^2})^2}}$ $\frac{1}{\mathcal{C}_b^2 \frac{\mathcal{K}_\mathcal{S}}{M}(1+\frac{\mathcal{N}^2}{\mathcal{K}_\mathcal{S}\mathcal{C}_b})} = \frac{\mathcal{R}_b^2}{\mathcal{R}_{Lopt}} \frac{1}{1+\frac{\mathcal{N}^2}{\mathcal{K}_\mathcal{S}\mathcal{C}_b}}$

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[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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4 0 8

[Presentation of the system](#page-14-0) [EMR of the system](#page-16-0) [Power Extraction on a load resistor](#page-17-0) R_L from harmonic oscillation

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4 **ED**

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For the realistic case, there is one or two resistive loads which allow to extract the maximum of power,

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- **•** For the realistic case, there is one or two resistive loads which allow to extract the maximum of power,
- **•** There exist an optimal frequency which may vary if R_L is very high,
- For highly damped structure, a simple resistor is not optimal.

 \rightarrow we always want to harvest the maximum of power!

Table of contents

[Introduction](#page-3-0)

- [What is Energy Harvesting ?](#page-3-0)
- **[Generator Technologies](#page-7-0)**
- **•** [Summary](#page-12-0)

2 [Modelling of a piezoelectric energy harvester](#page-14-0)

- **•** [Presentation of the system](#page-14-0)
- [EMR of the system](#page-16-0)
- **[Power Extraction on a load resistor](#page-17-0) R_L** from harmonic oscillation

3 [An Example of inverter](#page-30-0)

- **•** [Introduction](#page-30-0)
- **[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0)**

[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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and $v = -v_l = -R_l i_m$

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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 $v_L = R_L i_m$ which is > 0 and $v = -v_l = -R_l i_m$

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

4 0 8

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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$$
\lim_{i_m} \left\{\left\{\left\{\frac{1}{\sigma} \sum_{i=1}^{m} \sum_{j=1}^{n} \sigma_{ij} \right\}_{k} \right\}_{\nu_L}
$$
\n
$$
v_L = -R_L i_m \text{ which is } > 0
$$
\n
$$
v = v_L = -R_L i_m
$$

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Introduction

 $v_L = R_L i_m$ which is > 0 and $v = -v_l = -R_l i_m$

The current is rectified, but we still have $v = -R_L i_m$: Power harvesting depends on R_L

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$$
\lim_{i_m} \bigotimes_{u} \left[\frac{\sum_{i=1}^{i_m} \sum_{j=1}^{k_m} \sum_{j=1}^{k_m} \mathbf{r}_i}{\sum_{i=1}^{k_m} \sum_{j=1}^{k_m} \sum_{j=1}^{k_m} \mathbf{r}_i} \right]_{v_L}
$$
\n
$$
v_L = -R_L i_m
$$
\n
$$
v = v_L = -R_L i_m
$$

[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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4 **ED**

[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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4 **ED**

[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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The current is rectified, but we still have $v = -R_L i_m$: Power harvesting depends on R_L Moreover, it is still not optimal if $R_{opt} > R_b$. This is why, some want to compensate for C_b :

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$$
i_m < 0
$$

\n
$$
v_L = -R_L i_m
$$
 which is > 0
\n
$$
v = v_L = -R_L i_m
$$

[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Introduction

 $v_l = R_l i_m$ which is > 0 and $v = -v_L = -R_L i_m$

The current is rectified, but we still have $v = -R_l i_m$: Power harvesting depends on R_l Moreover, it is still not optimal if $R_{opt} > R_b$. This is why, some want to compensate for C_b :

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Why Synchronized

Strategy: $v = -R_{opt}i_m$ leads to $\frac{f_p}{N} = -\frac{D_s}{N^2}N\dot{w}$ or, $f_p = -D_s\dot{w}$.

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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Why Synchronized

Strategy: $v = -R_{opt}i_m$ leads to $\frac{f_p}{N} = -\frac{D_s}{N^2}Nw$ or, $f_p = -D_sw$. This shows that *v* should be controlled.

[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Why Synchronized

Strategy: $v = -R_{opt}i_m$ leads to $\frac{f_p}{N} = -\frac{D_s}{N^2}Nw$ or, $f_p = -D_s w$. This shows that *v* should be controlled.SSHI does this with efficiency.

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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How it works

LC oscillations

Frédéric Giraud [Master E2D2](#page-1-0) November 27, 2012 32 / 40

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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LC oscillations

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) **[Conclusion](#page-34-0)**

How it works

LC oscillations $v +$ i $t = 0$ *t v*, *i*

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) **[Conclusion](#page-34-0)**

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

How it works

LC oscillations **SWITC** Switched inductor $v +$ i $t = 0$ *t v*, *i*

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Frédéric Giraud [Master E2D2](#page-1-0) November 27, 2012 32 / 40

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

How it works

Switching is synchronized on \dot{w} , or

 $i_m = Nw$.

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

How it works

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Conclusion

Performances

• SSHI can extract energy more efficiently than a resistor when damping is important,

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Conclusion

Performances

- **SSHI** can extract energy more efficiently than a resistor when damping is important,
- But Power extraction still depends on the load,

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[Introduction](#page-30-0) [SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

Conclusion

Performances

- **SSHI** can extract energy more efficiently than a resistor when damping is important,
- But Power extraction still depends on the load,
- Needs to measure bender's deflection *w*(*t*).

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General conclusion

In this presentation, applications of Energy Harvesting were shown. The modelling of a piezoelectric generator has shown that the power source needs an adaptation:

- in frequency,
- in load.

to maximize the harvested poer.

The key energy management rules were presented through the analysis of the EMR of the system. A typical power electronic circuit was also presented, but the bibliography shows a lot of example.

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[SSHI: Synchronized Switch Harvesting on Inductor](#page-31-0) [Conclusion](#page-34-0)

End of the presentation

Questions?

Frédéric Giraud [Master E2D2](#page-1-0) November 27, 2012 37 / 40

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 298