

# Differential Structures

Damien Prêle

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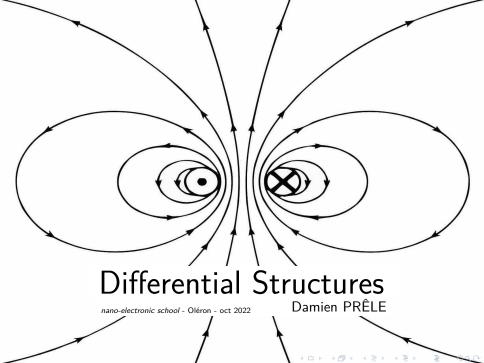
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## Introduction

### Differential transmissions

Differential signals Differential lines Coupling

## Differential amplifier

Single to differential Fully differential amplifier Differential pair with "transistor load" Common Centroid Layout

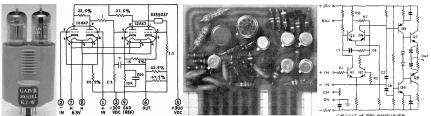
Noise and noise rejection





## Introduction: Initial use

- Differential structures since beginning of signal transmission
- Introduced to minimize response to common mode signals/noises/interferences
- Differential amplifier circuit using vacuum tubes in 1937/38
   (common-cathodes dual pentode circuit) used to drive push-pull
- ► Also introduced for "analog computing" in the 50s/60s to do mathematical operations in analog computers



GAP/R K2-W vacum tube and solid-state (model P45) op amps

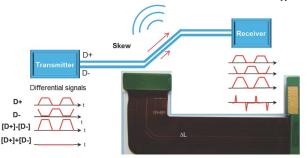


## Introduction: Reduce noise emissions

## Electromagnetic compatibility



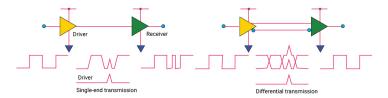
In our connected world, data exchange very fast ... include high-speed serial links, ... fast transition times and long lines may induce radiations due to common mode noise ... AN4511 Application note





# Introduction: Reducing common mode noise contamination

**Low-voltage differential signaling**, or LVDS, is a way to communicate data using a differential signal - reduce common mode noise contamination - with a small voltage swing: LVDS standardized as ANSI/EIA/TIA 644 offers gigabit speeds at very low power



Also true for small/low-noise analog signal transmissions ...





### Introduction

## Differential transmissions

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Fully differential amplifier
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Common Centroid Layout

Noise and noise rejection





# Differential signaling

To decouple transmitted signals from "references" and reject external perturbations/emissions:

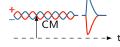
- balanced line / signal pair
- 2 conductors same type ≠ coaxial (return current connected GND)
- circuits interfacing balanced line must also be balanced :
  - transformer or ballun / autotransformer
  - differential to single or single to differential
  - floating sources or loads
  - differential sensors
- balanced impedances to ground
- wires twisted together → each conductor is equally exposed to noise-inducing magnetic fields
- + Maximum output is twice as much (wrt norm/standard)





opposite phase/polarity

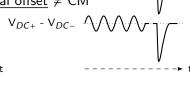
- both same amplitude
- could be also associated to a common mode "signal"



Differential signal characteristics

differential amplitude = twice larger than each opposite signal

can be affected by a differential offset ≠ CM





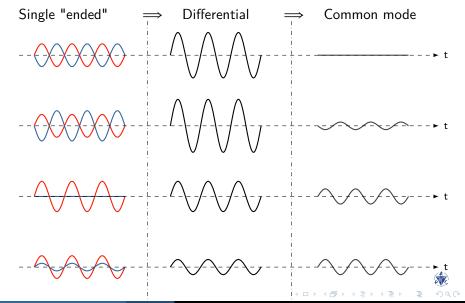
Single 
$$V_+$$
 and  $V_ \Rightarrow$   $V_{diff} = V_+ - V_ \Rightarrow$   $V_{CM} = \frac{V_+ + V_-}{2}$ 

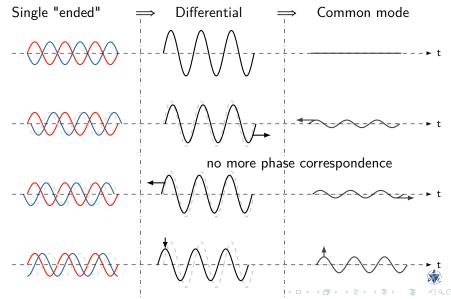
# Causes of imbalance on differential signals

- Lack of symmetry on the device pairs
- unbalanced biasing
- Differences in routing **length**
- Differences in routing widths
- Differences in routing resistivity
- Differences in routing layer/material
- Routing through non-continous grounding/return
- **Coupling** to other traces and grounding inhomogeneities
- Active devices **timing/BW** asymmetry
- unbalanced impedance/matching

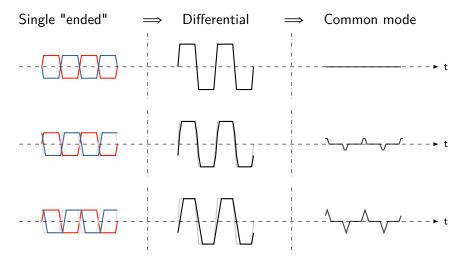


# Unbalanced amplitude: diff. to CM conversion





# Skewed: CM glitches & slow transient





# Balanced line/circuit and differential signaling

1. A balanced line/circuit shows a symmetry for common-mode rejection



2. Two wire transmission & "transposition" was introduced end of the 19th century to improve telegraph/telephone transmissions

in replacement of single-wire earth return affected by ... electric trams interference



3. It as also applied to tree phase power transmission lines to restrain induced current in parallel lines and for phase balancing



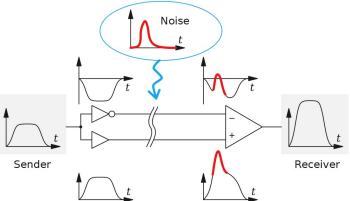


4. Twisted pairs - ethernet networks



# Differential signalling

Transmitting information using two complementary signals same, but opposite, electrical signal, each in its own conductor



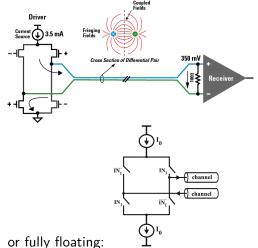
The pair of conductors can be wires in a twisted-pair or ribbon cable or traces on a printed circuit board...





# Differential signalling

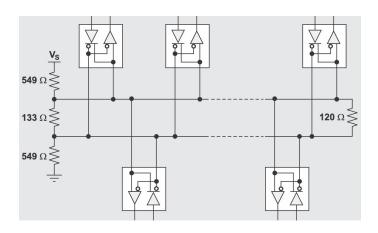
## LVDS:







## Failsafe mode: RS485

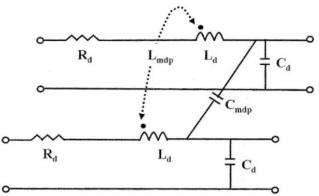


or 2 loads at 120  $\Omega$  and 800  $\Omega$  pull resistors can be also used ...



# Coupling of a differential line in planar technology

A transmission line couples with any references at direct proximity, as for example the complementary line

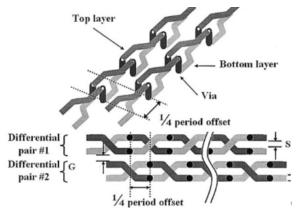






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# Differential twisted paire in planar technology

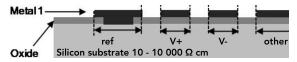


IEEE TRANSACTIONS ON ADVANCED PACKAGING, VOL. 27, NO. 4, NOVEMBER 2004, D. G. Kam et al.

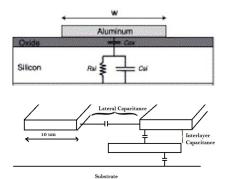
Twisted Differential Line Structure to Reduce Crosstalk and Radiated Emission



# Differential twisted pair in planar technology

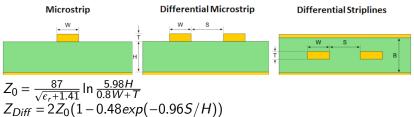


substrats resistance in the range 10 -  $10~000~\Omega$  cm -> qq  $\Omega$  to a reference

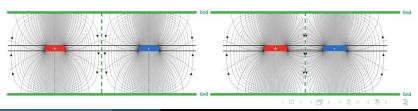




# Microstrip impedance : $Z_0$ single ended vs differential



Differential pairs are never tightly coupled together. Electric and magnetic fields from the signal and return paths of one transmission line couple to another and to the substrate.



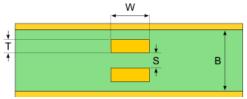


Tightly coupled (Spacing = w), loosely coupled (Spacing = 2w) and uncoupled pairs (Spacing = 3w), drawn to scale for 100 Ohm differential impedance



Tight or Loosely Coupled Differential Pairs to Reduce Cross Talk? Signal Integrity Journal

## Broadstriplines can also reinforce differential coupling:

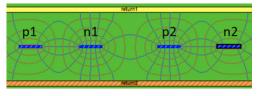






# Tight coupling and cross talk

Trying to tightly couple a differential pair increases the risk of cross talk



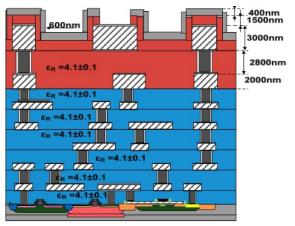
differential pairs with fringe fiend lines between adjacent channels





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# Dielectric constant and metal distances and thickness in a BiCMOS SiGe 130 nm technology



cross section showing thickness of the top two-layer metals layers and the relative permittivity (FR4 4.7, SiO2 3.9, Silicon 12)



## Differential amplifier

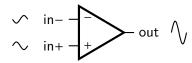
Single to differential Fully differential amplifier Differential pair with "transistor load" Common Centroid Layout



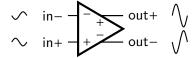


# What we call differential amplifier?

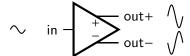
Differential input -> single ended output



but also ... Differential input -> differential output



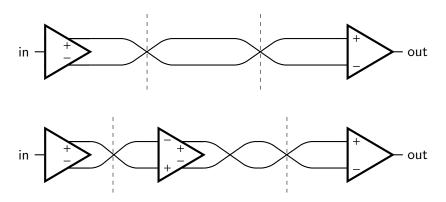
or could be ... Single "ended" input -> differential output







single to differential  $\Rightarrow$  differential signal  $\Rightarrow$  differential to single



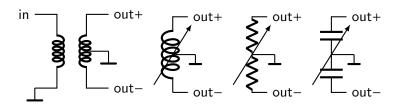
- 1. Single ended to differential (S2D)
- 2. Transmission line and differential to differential amplifier
- 3. Differential to single ended (D2S)



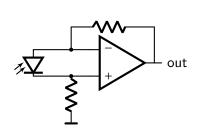
prele@apc.in2p3.fr

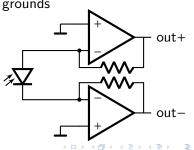
# Intrinsic differential signal: directely provide by the sensors

Center tap in transformer or in any devices (or with a dark one)



or connecting sensors with floating grounds

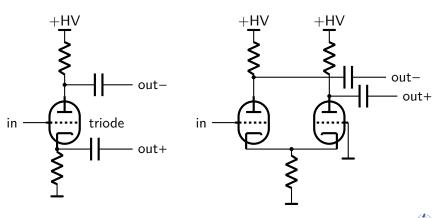






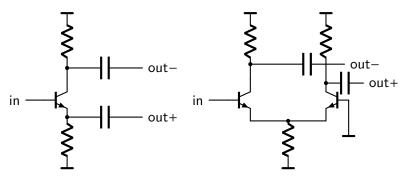
# Single to differential amplifier: phase splitter

Phase splitter stage of a push-pull vacuum tube amplifier, used during decades to drive "single type" push-pull + output transfo.



# Single to differential amplifier: phase splitter

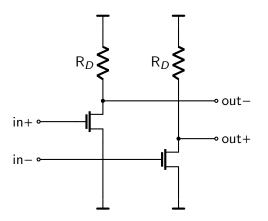
Phase splitter with solid state devices. producing two balanced voltage outputs of equal amplitude but opposite polarity



used to produce differential signaling



# Differential amplifier could be 2 single ended amplifier

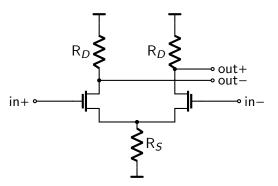


Double the dynamic, reject the Power supply Noise :-) ... but not strongly the common mode :-( =>  $G_{CM} \approx G_{Diff}$   $G_{Diff} = gmR_d$ ,  $G_{CM} = gmR_d/2$ , CMRR=2

Not easy to determined gm ... gm =  $\sqrt{2\mu_n C_{ox} I_D W/L}$  ... but  $I_D$ ?



# Differential pair



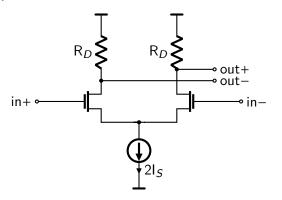
Double the dynamic, reject the Power supply Noise AND the common mode

 $G_{Diff} = gmR_D$ ,  $G_{CM} = R_D/2R_S$ , CMRR=gm2R<sub>S</sub>

Not easy to determined gm -> replace  $R_S$  by a current source 2  $I_D$  Output voltage and gain are linked and need high power supply for large gain



# Differential pair with current source



gm deduce from IS : gm =  $\sqrt{\mu_n C_{ox} I_S W/L}$  & larger CMRR Fully symmetric differential pair senses differential. A differential change in the inputs V+ and V- absorbed by Vgs1 and Vgs2 leaving middle voltage constant : virtual ground

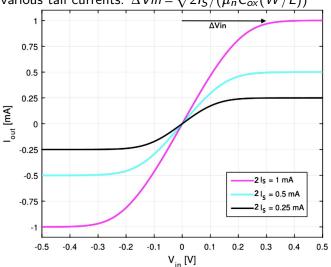
 ${\rm V}_D = {\rm V}_{dd} - {\rm I}_S \times {\rm R}_D -> {\rm gain\ limitation\ and\ output\ common\ mode\ link}\ \textit{We\ need\ a\ larger\ drain\ resistor\ to\ achieve}$ 



higher gain, but more drain resistance means a lower DC voltage at the output hodes

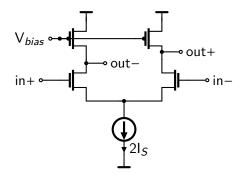
## Differential amplifier response

differential output current vs. the differential input voltage for various tail currents.  $\Delta Vin = \sqrt{2I_S/(\mu_n C_{ox}(W/L))}$ 





# Differential pair with current load



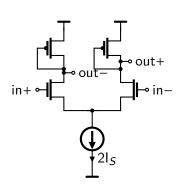
Decouple operating voltage and load impedance value.

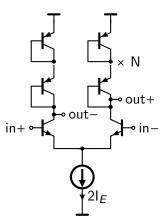
Allows larger gain with moderate power supply voltage.

Current sources :  $G_{Diff} \approx gm_N/r_{0_P}$  The input and output common mode voltage are "free" ... but have to be fixe by other "circuits"



# Differential pair with diode load

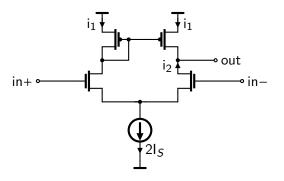




Diode Load :  $G_{Diff} \approx gm_N/gm_P \approx \sqrt{\mu_n W_N L_P/(\mu_p W_P L_N)}$  MOS : W/L to scale the gain (independent to bias and T) Bipolar :  $G_{Diff} \approx gm_{npn} \times 1/gm_{pnp} \approx N$  number of diodes (gm=qI<sub>C</sub>/kT independent to size)  $\rightarrow$  drift compensation & better linearity (in a given range)



# Single-ended differential pair with differential input: active load



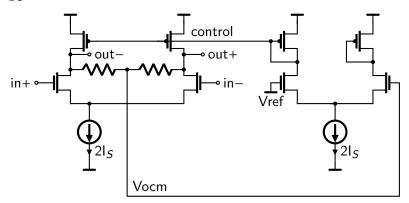
coupling of the  $I_D$  of each NMOS through a mirror  $i_1 = gm_N V_{in+} \ i_2 = gm_N V_{in-} \ V_{out} = (i_1 + i_2)(r_{0_N}//r_{0_P})$  "G\_Diff"  $\approx gm_N \ (r_{0_N}//r_{0_P})$ 

Output common mode must be similar to the PMOS diode D voltage.



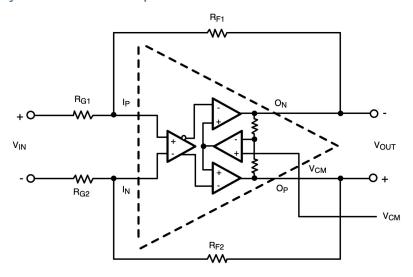
### Fully-Differential Amplifiers Common Mode Feedback

Output common mode voltage is measured and used to adjust the  $V_{DS}$  load ->  $V_{OS}$  load ->  $V_{OS}$  load ->  $V_{OS}$ 





## Fully-Differential Amplifiers Common Mode Feedback



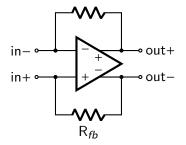
AN-1719 Noise Figure Analysis Fully Differential Amplifier



## Fully-Differential Amplifiers with feedback

Miller effect:  $Z_{in} = 2R_{fb}/(1+G_{Diff})$ 

- ightharpoonup R<sub>fb</sub>/G<sub>Diff</sub> < 50  $\Omega$  Trans-impedance amplifier
- $ightharpoonup R_{fb}/G_{Diff} = 50 \ \Omega$  Active low noise impedance matching

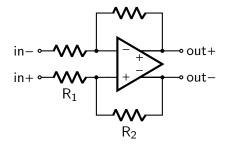






## Fully-Differential Amplifiers with feedback

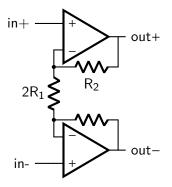
Intrinsic differential gain is often "proportional" to I and T -> To fix gain  $R_2/R_1\,$ 



if the intrinsic gain is large :  $G_{Diff} = R_2/R_1$   $Z_{in} \approx 2R_1$ 



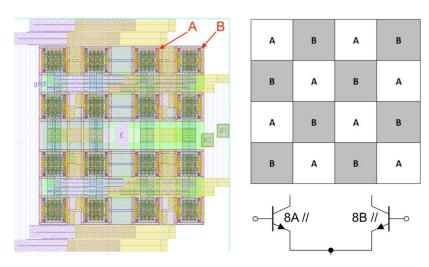
### Fully differential instrumentation-like amplifier



 $G_{Diff} = R_2/R_1$  High differential input impedance

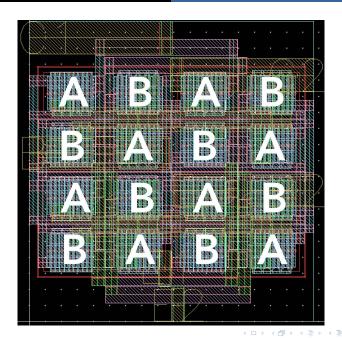


### Balancing = Common Centroid Method



Si Chen PhD https://tel.archives-ouvertes.fr/tel-02871901/









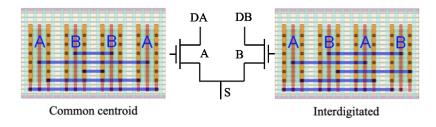
### For not square: ABBA preferred







### For not square: ABBA preferred

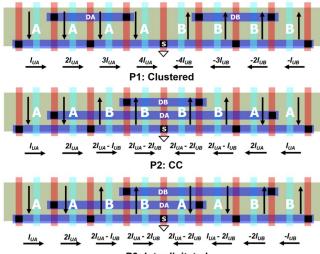


Common-Centroid Layouts for Analog Circuits: Advantages and Limitations - A. K. Sharma et al.





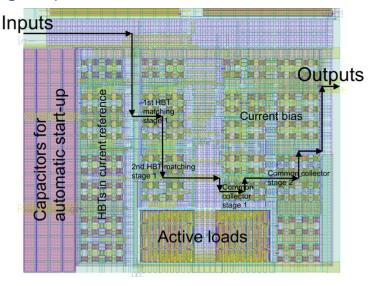
# Clustered, Common-centroid and InterDigitated layouts with routing connections



P3: Interdigitated



### Following the pair



Si Chen PhD https://tel.archives-ouvertes.fr/tel-02871901/

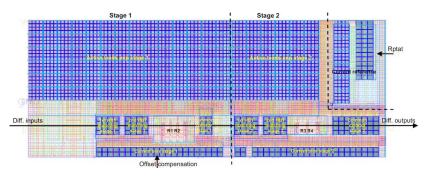


Si Chen PhD https://tel.archives-ouvertes.fr/tel-02871901/



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### Crossing pairs in a straight line



Si Chen et al. Monolithic amplifier and current biasing for SQUID readout AwaXe v4 - 2022



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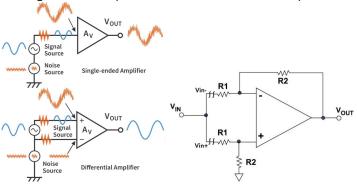
### Noise and noise rejection





## Common Mode Rejection Ratio Measurement - CMRR

Same signal applied to both inputs of differential device Average of the outputs in case of differential output  $\neq$  differential signal



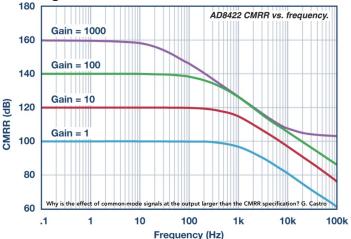
$$CMRR = \frac{\text{differential-mode gain}}{\text{common-mode gain}}$$
 
$$CMRR = \frac{G_{Diff}}{G_{CM}} = \frac{V_{out}/(Vin+Vin-)}{\Delta V_{out}/\Delta V_{in}} = \frac{R2/R1}{\Delta V_{out}/\Delta V_{in}} = \frac{R2/R1\Delta V_{in}}{\Delta V_{out}}$$





# CMRR(f)

Common mode rejection decrease with frequency and depends the differential gain







# $\sqrt{2}$ noise more ?

Input noise is quadratically summed at the 2 inputs ... but signal is double !

SNR in increased by a factor of  $\sqrt{2}$  in differential for same amplitude signal at each end



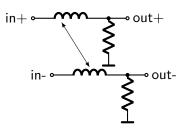


### Common Mode Filters

### Differential topology

- with good symmetry and balancing
- with virtual ground and differential impedances

Allows Common Mode Rejection and Power Supply Rejection ... Moreover, it exist filters allowing attenuation of the Common Mode, with no attenuation of the Differential signal Common mode filter are inductive filter like LR low passe filter:



$$f_c = \frac{1}{2\pi L/R}$$
 -> with 50  $\Omega$ , L must be  $=\frac{50}{2\pi f_c} = 8~\mu H|_{f_c=1MHz}$ 



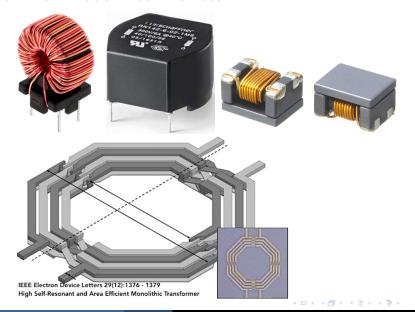
54 / 58

# Common Mode Filters Principle

Can reduce the external noise and the CM noise induced by skew on a differential link

can also be use as a "differential filter" :

### Common Mode Filter Devices



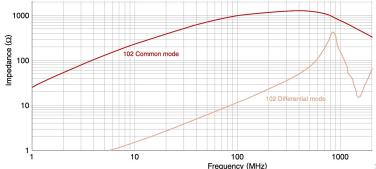
# Common Mode Filtering Impedance

Common mode impedance increase with f as  $L\omega$  (ACP3225)

Common mode impedance [at 100MHz]		DC resistance		Rated current*	Rated voltage	Insulation resistance
<b>(Ω)</b>	Tolerance	(m $\Omega$ )typ.	$(m\Omega)$ max.	(A)max.	(V)max.	(M $\Omega$ )min.
1000	±25%	50	100	1.5	60	10
500	±25%	40	100	2	60	10

Other with thin wire exhibit high resistance not compatible with 50  $\Omega$  matching : 3k  $\Omega$  @ 500k  $\Omega$  & DC resistance 2 k  $\Omega$  (ST-101A )

Finaly, the best is to have the impedance in CM and differential as function of frequency :





### Conclusion

- Common Mode Rejection
  - Common Mode Noise Rejection: use-full especially for transmission of signal over significant distances
  - Return current to ground is near zero reducing ground bounce issue
  - Ease the DC coupling between stages
- Twice the amplitude and improve signal to noise
  - Vpp is twice the voltage amplitude of one end. Especialy interesting with the decrease of ASIC technology power supply. Again, for transmission to an other stage ...
  - However the differential structure twice the circuit area and need 2 times more current
  - ▶ The noise is also multiply by  $\sqrt{2}$  ... but the SNR is still improve
- ► <u>Also:</u> reduce glitches on supply if well balanced ...

The real interest depend the application: long transmission line with larger sensitivity to external noise sources and less well define references ... less interesting for low consumption compact readout

